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CATIA V5 Structural Analysis for the Designer

CAT509 Workshops

March 2002



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WORKSHOP 1

FEM REVIEW









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WS1-1

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- Quiz yourself on the FEM:
 - 1. How can preliminary structural analysis improve the design process?
 - 2. Briefly describe the Finite Element Method (FEM).

- 3. Simple pieces that represent a more complex structure are called
- 4. The simple pieces mentioned above are connected together at
- 5. The assembly of #3 and #4 is called a ______



- Quiz yourself on FEA:
 - 1. What are the six main steps in pre-processing a finite element analysis (FEA)?
 - 2. Name a load type that would be applied in FEA.
 - 3. Name a constraint (restraint) type that would be applied in FEA.
 - 4. What step in FEA comes between pre- and post-processing?
 - 5. What are the two main steps in FEA post-processing?
 - 6. How are FEA results displayed?



- Quiz yourself on CATIA structural analysis:
 - 1. What are the 3 types of analysis supported by the CATIA structural analysis tools?

2. Write the name or sketch at least one linear and one parabolic element supported by the CATIA structural analysis tools.

3. What is the name of your instructor? (extra credit)



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WORKSHOP 2

FOOT PEG





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Problem Description

- A new All Terrain Vehicle (ATV) is being designed to carry two people – a driver and a passenger. An area of concern is the Foot Peg for the passenger on the ATV. The Foot Peg needs to be small due to limited space on the ATV yet able to handle the force of the passenger during the ride.
- Analyze the Foot Peg as an aluminum part in the preliminary design phase to check for part failure in a static condition.





Suggested Exercise Steps

- 1. Open the existing CATIA part in the Part Design workbench.
- 2. Apply aluminum material properties to the part.
- 3. Create a new CATIA analysis document (.CATAnalysis).
- 4. Apply the restraint condition.
- 5. Apply the load condition.
- 6. Compute the analysis.
- 7. Visualize the analysis results.
- 8. Save the analysis document.



Step 1. Open the part

Open the Foot Peg part in the Part Design workbench.

Steps:

1. Select File and Open... from the top pull-down menu.

2. Access the class workshop directory using the typical Windows interface.

3. Open the ws2footpeg.CATPart by double-clicking.

By default, the Foot Peg and any other CATPart document is opened in Part Design workbench.





Step 2. Apply material properties



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Step 2. Apply material properties

🛐 CATIA V5 - [Foot Peg.CATPart]

🌄 <u>S</u>tart Team<u>P</u>DM <u>F</u>ile <u>E</u>dit - 8 × Tools Window Help View Insert 🛐 Foot Peg Toolbars - 🖉 🖉 🖉 腧 Render Style Wireframe (NHR) 🖉 yz plane Navigation Mode Dynamic Hidden Line Removal - 🗾 🗾 🗾 🖉 📲 Relations Lighting... Shading (SHD) **Custom View Modes** ? × 🐏 <u>PartBodv</u> Depth Effect... Shading With Edges Apply the customized ⊢🕖 Pad.1 Edges_points Ground Shading With Edges And Hidden Ed render mode to view Pocket.1 🧧 Shading 🔍 Magnifier... Apply Customized View the Aluminum material Pocket.2 Outlines Hide/Show display. Customize View - 🛗 RectPattern Hidden edges_points Full Screen Steps: - Material=Aluminium Dynamic hidden line removal 1 Aluminium 1. Click the 📕 Materials 2 **Customized View** 3 Facet **Parameters** Isoparametrics Material property seen icon. in the specification tree 🎱 🔒 ОК 👘 🥥 Cancel 2. If material display is not seen. select Customize View under 4 Render Style from the View pull-down menu. P ₩ 3. Activate the $[\mathbf{0}]$ Materials box in the ٦ **Custom View Modes** 1 F1 definition window. Ħ 4. Click OK. 🗋 🛎 🖶 👙 🗴 🖻 🖏 🗠 🛠 🕽 ╦ 竹 🎚 🖻 粥 品 整 、 品 整 🤹 🥸 🤤 🔍 🔍 🔔 🗇 🛢 fю 🔳 🐗 👌 🚰 🦂 🍓 🧯 CATIA P2 Select an object or a command

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WS2-7



- 8 ×

Create a CATAnalysis document that will contain the information for our static analysis of the Foot Peg.

Steps:

1. Select the GSA workbench from the Start menu.

2. Highlight the Static Analysis case.

3. Click OK.

The new CATAnalysis document is now active in the GSA workbench.



WS2-8

SOFTWARE

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Step 4. Apply restraint condition



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Steps:

Step 4. Apply restraint condition



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Step 5. Apply load condition

Apply a force load of 550lbf to the Foot Peg top face in a direction normal to the face pushing downward.

Steps:

1. Select the force icon from the GSA 5℃ workbench.

2. Drag and drop the compass on to the top face to establish an axis system normal to the face.

3. The top face is highlighted and force vectors shown.

4. Key in value -550lbf for the Z vector...OK.





Step 5. Apply load condition



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The force load is created and seen in the specification tree.

The force load is applied to the top face in a downward direction as shown by the vector arrows.

Hint: Drag and drop the compass back to its normal position away from the part after use.

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Step 6. Compute the analysis



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Steps:

icon.

Step 7. Visualize analysis results



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Step 7. Visualize analysis results



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Step 8. Save analysis document



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Save the analysis

document.

1. Select Save

2. Highlight the

CATAnalysis

button.

Steps:

WS2-16



Step 8. Save analysis document



4. Select the directory path.

5. Key in Foot Peg Static for the analysis document name.

6. Click Save.

7. Notice the new name and Action "Save" for the analysis document.

8. Click OK to execute the noted Actions.



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WORKSHOP 3

BICYCLE PEDAL STATIC ANALYSIS





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Problem Description

- Your job will be to analyze various components of a mountain bicycle. We will start with the pedal.
- Let's assume a 200 lb person riding this bike is standing, balanced evenly on each pedal. Material (Steel) properties as specified below. Use a rough analysis to determine where the high stress areas exist that will require additional mesh refinement.





Suggested Exercise Steps

- 1. Open the existing CATIA part in the Part Design workbench.
- 2. Apply steel material properties to the part.
- 3. Create a new CATIA analysis document (.CATAnalysis).
- 4. Pre-process initial finite element mesh.
- 5. Apply a clamp restraint.
- 6. Apply a distributed force.
- 7. Compute the analysis.
- 8. Visualize the analysis results.
- 9. Save the analysis document.







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WS3-4

Step 1. Open the existing CATIA part



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Step 2. Apply steel material properties to the part



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WS3-6

Step 2. Apply steel material properties to the part



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WS3-7



Step 2. Apply steel material properties to the part



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Step 3. Create a new CATIA analysis document



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WS3-9

Step 3. Create a new CATIA analysis document



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WS3-10

Step 4. Pre-process initial finite element mesh





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WS3-11

Step 5. Apply a clamp restraint





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Step 6. Apply a distributed force





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Step 7. Compute the analysis



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WS3-15

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WS3-19

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WS3-20

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Conclusions

- You now know where the "hot spots" are but the stress and displacement results are questionable with a 43.5% Global Precision Error.
- The next step is to refine the mesh in the critical areas. We will go over this in the next workshop #4.

	.25" Linear Mesh
Max Von Mises	24.6 ksi
Translational Displacement	.00407 inch
Error Estimate	8.65e-8
Global % Precision error	43.5 %
Local % Precision error	NA %

	Recommendation
Error Estimate	1.00e-8 (zero)
Global % Precision error	20 %
Local % Precision error	10 %





Step 9. Save the analysis document

Stone:	CATIA V5 -	- [ws3pedal.CATAnalysis]			
<u>Steps.</u>	Start Te	eam <u>P</u> DM <u>File E</u> dit <u>V</u> iew	<u>I</u> nsert <u>T</u> ools		
1. From the File menu		<u>N</u> ew	Ctrl+N		
select Save		Ne <u>w</u> from			
Management.		2 Open	Ctrl+O		
2. Select document		Close			
you want to save.					
3. Select Save As to		Save	Ctrl+5		
specify name and	_	Save <u>A</u> s			
path, select OK.		Save All			
The pedal.CATPart		Sa <u>v</u> e Manager	ent		
and .CATAnalysis					3
should each be saved			2		
under a new name in					
the work directory.					
Save Management					?×
State	Name	Path		Action	Save
Modified	ws3pedal.CATPart	C:\CATIA\Training\(C:\Preserver Files\De	data 	Save Auto	Save As
New	ws3pedal.CATAnalysi	is C:\CATIA\Training\a	issault Systemes(607(intel_a(s data	tartup(materiais Save	Propagate directory
Opened	pedal.CATAnalysisRe:	sults C:\ELFINI\pedal			Reset
Opened	pedal.CATArialysisCol	піросас С: (ссітлятурецаі			
0 Unsaved File(s) Left		Enable in	idependent saves		
					OK Scancel
AT509, Workshop 3, Ma	rch 2002	WS	63-22		MSCSOFTWA

WORKSHOP 4

BICYCLE PEDAL MESH REFINEMENT AND ADAPTIVITY





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Problem Description

- Assume the same 200 lb person riding the bicycle is standing balanced evenly on each pedal. Material (Steel) properties are as specified below.
- Using the previous rough analysis, refine the mesh until you are comfortable with the results. Is this steel strong enough?

01001710	1017100	
Elastic Modulus, E	29.0E6 psi	
Poisson's Ratio, v	0.3	
Density	.284 lb/in ³	100 lbs
Yield Strength	36,000 psi	Bart
	100 lbs	Contraction of the second seco





WORKSHOP 4 – PEDAL MESH REFINEMENT AND ADAPTIVITY

Suggested Exercise Steps

- 1. Open the existing CATIA analysis in the GSA workbench.
- 2. Change mesh to parabolic and add local meshing.
- 3. Compute the more precise analysis.
- 4. Search for point(s) of maximum Von Mises stress.
- 5. Search for point(s) of minimum precision.
- 6. Visualize the refined analysis results.
- 7. Create an adaptivity box with a 5% target.
- 8. Adapt and converge.
- 9. Visualize the adaptive analysis results.
- 10. Verify reactions.
- 11. Generate a basic analysis report.
- 12. Save the analysis document.







Step 1. Open the existing CATIA analysis



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Step 1. Open the existing CATIA analysis





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Step 1. Open the existing CATIA analysis



Step 2. Change mesh to parabolic and add local meshing



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Step 2. Change mesh to parabolic and add local meshing



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Step 2. Change mesh to parabolic and add local meshing



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Step 3. Compute the more precise analysis



Step 4. Search for point(s) of maximum Von Mises stress



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Step 5. Search for point(s) of minimum precision





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Step 6. Visualize the refined analysis results



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Step 7. Create an adaptivity box with a 10% target





Step 8. Adapt and converge



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WS4-21

Step 10. Verify reactions



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WS4-22
Conclusions

- The load set of a 200 lb man will overstress the pedal made of A36 steel. Use 4340 material and heat treat to 260-280 BHN for a yield strength equal to 217 ksi. You must change the material type and characteristics in the .CATPart document.
- To add a different material to the CATIA material selector material catalog see Info Nugget – Materials Catalog.



or to create your own

	.25" Linear Mesh, .025 sag	.25"Linear Global Mesh, .025" sag .125" Parabolic Local Mesh, .013" sag Adapt and converge target of 5% locally	
Max Von Mises	24.6 ksi	172.3 ksi	
Translational Displacement	.0047 inch	.00562 inch	
Error Estimate	8.65e-8 Btu	8.4e-16 Btu local	
Global % Precision error	43.5 %	18.1 %	
Local % Precision error	NA %	12.4 %	



Step 11. Generate a basic analysis report



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WS4-24

Step 12. Save the analysis document



Info Nugget – Running with the Intel MKL Library



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WS4-26

Info Nugget – Running with the Intel MKL Library

System Properties System Restore General Computer Na	Automatic Updates Remote Memory Advanced			
You must be logged on as an Ac Performance Visual effects, processor scheo User Profiles Desktop settings related to you Startup and Recovery Sustem startup, sustem failure.	Ininistrator to make most of these changes.	nment Variables or variables for Jack Kosydar ariable Value EMP C:\Documents and Setti MP C:\Documents and Setti NP Ed	? X ings\Jack Kosyd ings\Jack Kosyd it Delete	
To activate library, add Intel address to your system "Path". <u>Steps:</u> 1. Select start + Control Panel + Performance and Maintenance + System + Advanced +	Settings Settings ent Variables Error Reporting OK Cancel Apply	tem variables ariable OMSpec C:\WINDOWS\system32 UMBER_OF_P S Windows_NT ath C:\WINDOWS\system32 ATHEXT .COM;.EXE;.BAT;.CMD; New Ed	2\cmd.exe 2 ;C:\WINDOWS; .VBS;.VBE;.JS; it Delete OK Cancel	2
Environment Variables. 2. Select "Path" in the System variables, then Edit. 3. Add location to the "path", select OK, OK, OK. 4. Reput	Computation Resources Estin 1e+002 s of CPU 1.3e+004 kilo-bytes of memor 7.37e+004 kilo-bytes of disk Intel MKL(c) Library found: Int Do you want to continue the co	Edit System Variable name V Variable value Variable value	n Variable me: Path lue: \System;C:\Prog	? × ram Files\Intel\plsuite\bin OK Cancel
CAT509, Workshop 4, March 2002	WS4-	-27		MSCSOFTWARE

Info Nugget – Paging Space

1 → 5	ystem Properties		1	<u> × </u>		Vir	rtual Memory			? ×
	System Restore General C You must be logged Performance Visual effects, proc	Automatic Computer Name on as an Administrator I essor scheduling, memo	Updates Hardware Advanced to make most of these changes. and virtual memory Settings			ſ	Drive [Volume Label] C:	Pagin	ig File Size (MB) 1000 - 2000	
Increasing you	User Profiles Desktop settings re Startup and Recove System startup, sys	lated to your logon ery tem failure, and debugg	Settings ing information Settings	Visu.	Adjust for best performance		Drive: C Space available: 4 Custom size: Initial size (MB): Maximum size (MB): [C System managed size	2: 1000 2000		3
space. Steps: 1. Select start Panel + Perfor and Maintenar System + Adva Performance S	+ Control rmance nce + anced + Settings.	Environment Variable	Error Reporting		Memory usage By default, the computer is se memory to run your programs Adjust for best performance Programs		 No paging file size for Minimum allowed: 2 Recommended: 7 Currently allocated: 1 	all drives 2 MB 766 MB 1000 MB	ок	Cancel
 Select Adva Virtual memory Change. If you have paging file size from 1GB to 2 Select OK, etc. 	anced + y room set e range GB. OK, OK.	CATIA e "not end	error note will ough memory	be	A paging file is an area on the f it were RAM. Total paging file size for all dr	e har ives: 2	d disk that Windows uses	as		

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Info Nugget – Batch Computing



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WS4-29

Info Nugget – Material Catalog

	Save Management							
	State	Name	Path					
	Opened	ws3pedal.CATAnalysis	C:\CATIA\Training\data					
	Opened	pedal.CATAnalysisResults	C:\ELFINI\pedal					
	Opened	pedal.CATAnalysisComputations	C:\ELFINI\pedal					
	Opened	ws3pedal.CATPart	C:\CATIA\Training\data					
•	Opened	Catalog.CATMaterial	C:\Program Files\Dassault Systemes\B07\intel_a\startup\materials					

_ 8 × 😽 CATIA V5 - [Catalog.CATMaterial] 🛐 <u>S</u>tart Team<u>P</u>DM File Edit <u>V</u>iew Insert Tools Window <u>H</u>elp _ 8 × Construction Fabrics Metal Other Stone Wood 2 Glossy Floor Concrete Floor Grate Hexagonal Tiling 1 **a**b 8 Kitchen Floor Marble Paving No Skid Pavement Plaster 3 ٩ ab PVC Turf Road Roughcast Tarmac AT Wall of Bricks Wall of Castle Wall of Stones Wood Floor

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Edit the existing **013** material catalog.

1

Steps:

1. Locate the existing Catalog.CATMaterial file by Selecting File + Save management. The path will show if "Link to File" was selected when applying material.

2 Open the file in a CATIA session. The Material Library workbench will start.

3. Edit this file with the various tools provided and save.

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WS4-30

Info Nugget – Personal Material Catalog



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CRANK ANALYSIS USING VIRTUAL PARTS







WS5-1

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Problem Description

 The same 200 lb person riding this bike, standing balanced evenly on each peddle. Determine if the Crank material is capable of carrying this load.





Suggested Exercise Steps

- 1. Open the existing CATIA part in the Part Design workbench.
- 2. Apply aluminum material properties to the part.
- 3. Create a new CATIA analysis document (.CATAnalysis).
- 4. Mesh globally with linear elements.
- 5. Apply a clamp restraint.
- 6. Simulate the pedal using a Smooth Virtual Part.
- 7. Apply a force to the Smooth Virtual Part.
- 8. Compute the initial analysis.
- 9. Visualize "hot spots" in the initial results.
- 10. Change mesh to parabolic and add local meshing.
- 11. Compute the more precise analysis.
- 12. Search for extrema points (max Von Mises, min precision).
- 13. Check local precision using adaptivity boxes.
- 14. Visualize final results (translations relative to user axis).
- 15. Save the analysis document.



WORKSHOP 5 – BICYCLE CRANK

2D DIAGRAM AND HAND CALCULATIONS

 Assume all 6 D.O.F. are restricted (clamped) where the crank attaches to the shaft.





 $Moment = P \cdot L = 100 lbs \cdot 6.75 inches = 675 inlbs$ $Bending = \frac{M \cdot c}{I} = \frac{675 inlbs \cdot 0.508 inches}{0.0446 in^4} = 7688 psi$ $Shear = \frac{T \cdot c}{J} = \frac{450 inlbs \cdot 0.341 inches}{0.0416 in^4} = 3689 psi$ $Combined = \frac{\sigma_x + \sigma_y}{2} + \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau^2_{xy}} = \frac{7688 psi}{2} + \sqrt{\left(\frac{7688 psi}{2}\right)^2 + 3689 psi^2} = 9172 psi$



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Step 1. Open the existing CATIA part

Statt TeamPDM File Edit	View Insert Tools			
	Ctrl+N			
Ne <u>w</u> fr	om	lection	? >	<u> </u>
1 📂 📴 Open	. Ctrl+0 Look jr	n: 🔁 catia	🗹 🖻 🖆 🔳	
Llose	Der 📃 Der	nos		
	Trai	ining		
	2 File Selection			? ×
	Look in:	🗁 data		
Open the CATIA part		Surges del Cattent		
the Part Design		🚮 ws3pedal.CATAnalysis	🚮 ws7seat.CATPart	
workbench.	My Recent	ws5CRANKassy.CATProduct	👼 ws7seatPost.CAT/	
Steps:	3	Wws5crankL.CATAnalysis	🚳 ws7seatPOSTassy 🚳 ws7unnerClamp.C.	
1 From the File menu			ws11front_wheel_	
select Open.	Desktop	Wws5wheel.CATPart	🔊 ws12shaft.CATPar	FIG
2 Access the class		ws5wheer_sider.carpart	Silves13fender.CATP.	
workshop directory	Mu Documents	ws6rearRack.CATPart		
using the typical	ing boomining	📓 ws7bolt.CATPart 📓 ws7lowerClamp.CATPart		
Windows interface.		ws7post.CATPart		
3. Open the crank by	My Computer	•	F	
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Design workbench.				

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WS5-6

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Step 2. Apply aluminum material properties to the part



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WS5-7

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Step 2. Apply steel material properties to the part



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WS5-8

Step 3. Create a new CATIA analysis document





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Step 3. Create a new CATIA analysis document





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Step 4. Mesh globally with linear elements





Step 5. Apply a clamp restraint





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Step 6. Simulate the pedal using a Contact Virtual Part



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WS5-13



Step 6. Simulate the pedal using a Smooth Virtual Part



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Step 7. Apply a force to the Smooth Virtual Part





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Step 8. Compute the initial analysis



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Step 9. Visualize "hot spots" in the initial analysis





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Step 9. Visualize "hot spots" in the initial analysis





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WS5-19



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WS5-20



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WS5-21



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WS5-22

Step 11. Compute the more precise analysis



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WS5-23

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Step 12. Visualize extremas





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Step 12. Visualize extremas





Step 13. Specify adaptivity boxes



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WS5-26
Step 14. Visualize final results



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WS5-27



Step 14. Visualize final results



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WS5-28

Step 14. Visualize final results



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WS5-29

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Conclusions

• New material is required with a yield strength higher than 15.3 ksi.

Hand Calc's: 9.17 ksi Combined Stress	.25" Linear Mesh, .025 sag	.25" Parabolic Global Mesh, .025" sag. .125" Parabolic Local Mesh, .013" sag. Adapt and converge not necessary.
Max Von Mises	8.30 ksi	15.3 ksi
Translational Displacement	? inch	0916" Z - direction at point of load
Error Estimate	1.01e-6 Btu	5.7e-8 Btu local
Global % Precision error	42.5 %	7.3 %
Local % Precision error	NA %	7.9 % and 3.7%



Step 15. Save the analysis document



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WS5-31



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WORKSHOP 6

REAR RACK (MODAL) ANALYSIS



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WS6-1



CAT509, Workshop 6, March 2002





Problem Description

- Assume the dynamic characteristics of this bike with a 200 lb person traveling at 40 mph down a cobble stone road is: Mode 1=95 Hz, Mode 2 = 100 Hz, Mode 3 = 110 Hz, Mode 4 = 120 Hz, Mode 5 = 135 Hz.
- A rear rack accessory capable of supporting 150 lbs may be attached to the frame. You are asked to analyze this rack under dynamic loading.
- Perform a normal modes analysis to determine if the frequency of the bike is close to one of the natural frequencies of the rack. This is to avoid excessive vibrations and find "soft spots" (smooth, comfortable ride).

Aluminum		
Elastic Modulus, E	10.15E6 psi	
Poisson's Ratio, v	0.346	
Density	.098 lb/in ³	
Yield Strength	13,77 <mark>8 psi</mark>	





Suggested Exercise Steps

- 1. Open the existing CATIA part in the Part Design workbench.
- 2. Apply aluminum material properties to the part.
- 3. Create a Frequency analysis document (.CATAnalysis).
- 4. Pre-process initial finite element mesh.
- 5. Apply a clamp restraint.
- 6. Apply a mass equipment load.
- 7. Compute the analysis.
- 8. Visualize the analysis results.
- 9. Generate a report of the results.
- 10. Save the analysis document.



Step 1. Open the existing CATIA part









Step 2. Apply aluminum material properties to the part



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WS6-6

Step 3. Create a Frequency analysis document



MSC

Step 3. Create a Frequency analysis document





MSC

Step 4. Pre-process initial finite element mesh



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WS6-9

MSC

Step 4. Pre-process initial finite element mesh



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WS6-10

MSC

Step 5. Apply a clamp restraint



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Step 6. Apply a mass equipment load



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WS6-12

MSC

Step 7. Compute the analysis





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Step 7. Compute the analysis





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WS6-15





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WS6-17

MSC



MSC

Step 9. Generate a report





MSC

Conclusions

 Comparing the natural frequency of the first 5 dynamic mode shapes shows a large difference. This verifies that we will have smooth ride "soft spots" during this load case.

Mode Number	Bike Frequency Hz (cycles/sec)	Rack Frequency Hz Parabolic Elements
1	95	9.47
2	100	9.71
3	110	31.66
4	120	40.50
5	135	61.36





Step 10. Save the analysis document





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WORKSHOP 7

SEAT POST ASSEMBLY ANALYSIS





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WS7-1



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Problem Description

- The sales department has informed engineering that the seat post keeps breaking.
- Perform an assembled static analysis to determine why and recommend a solution. Be conservative by using a design case of 200 lbs forward on the seat.

Post is Aluminum

Elastic Modulus, E	10.15E6 psi
Poisson's Ratio, v	0.346
Density	.098 lb_in3
Yield Strength	13,778 psi

Lower and Upper clamp is Steel

Elastic Modulus, E	29.0E6 psi
Poisson's Ratio, v	0.3
Density	.284 lb_in3
Yield Strength	<mark>3</mark> 6,000 psi



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Suggested Exercise Steps

- 1. Open the existing CATIA product in the Assembly Design workbench.
- 2. Apply material properties to all parts.
- 3. Examine and verify assembly constraints.
- 4. Create an assembly static analysis document (.CATAnalysis).
- 5. Pre-process initial finite element mesh.
- 6. Apply Property Connections.
- 7. Apply a clamp restraint.
- 8. Apply a moment load.
- 9. Compute the analysis.
- 10. Visualize the analysis results.
- 11. Compute a Frequency (Modal) analysis for the assembly.
- 12. Generate a report.
- 13. Save the analysis document.
- 14. Appendix showing precise results.





Step 1. Open the existing CATIA product (assembly)







Step 2. Apply material properties to all parts



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WS7-6

Step 3. Examine and verify assembly constraints



WS7-7

MSC

Step 3. Examine and verify assembly constraints



MSC
Step 3. Examine and verify assembly constraints



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Step 4. Create an assembly static analysis document



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WS7-10

MSC

Step 4. Create an assembly static analysis document



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Step 5. Pre-process initial finite element mesh



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Step 6. Apply Property Connections



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WS7-13

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WS7-20

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Step 8. Apply a moment load



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WS7-22

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WS7-23

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WS7-25

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WS7-30

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WS7-38

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MSC



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WS7-41



Window

Help

CATIA V5 - [ws7seatPostASSY.CATAnalysis]

Conclusions:

Maximum stress exceeds material yield. Select new material with yield values that exceed the analyzed Von Mises extrema using the parabolic element results.

	Von Mises extrema Linear elements, 44.5% precision	Von Mises extrema Parabolic elements, 9.8% precision
Post	58.0 ksi	98.2 ksi
Lower Clamp	72.8 ksi	144 ksi
Upper Clamp	41.6 ksi	101 ksi





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Step 12. Generate a report





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SEAT POST ASSEMBL ..

Frequency Case - Mic..
Step 12. Generate a report

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SEAT POST ASSEMBLY		
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Connectivity Statistics	BOUNDARY CON	DITIONS
SPIDER 506 (0.95%) TE4 52726 (99.05%)		
ELEMENT QUALITY:		
Criterian Gend Poor Bad Wr Skewness 51875 (98.39%) 848 (1.61%) 3 (0.01%) 0 (0.01%)		
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		Address 🖗 file:///CLFB&/readFoot/pope3.html#0
		FREQUENCY CASE
	STRUCTURE COM	BOUNDARY CONDITIONS
	Done .	
Results by selecting SEAT POST ASSEMBLY, Static Case and Frequency Case in the		
navigation.html.		
AT509, Workshop 7, March 2002	WS7-45	MSCSOFTWARE

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Step 13. Save the analysis document



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Von Mises "Lower Clamp" Extrema with Parabolic elements





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Von Mises "Upper Clamp" Extrema with Parabolic elements



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RECTANGULAR SECTION CANTILEVER BEAM





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WORKSHOP 8 – RECTANGULAR CANTILEVER BEAM





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Problem Description

- Hand Calculations
- Displacement:

t:
Moment of Inertia =
$$I_p = \frac{b \cdot d^3}{12} = \frac{1 \operatorname{inch} \cdot 2^3 \operatorname{inch}}{12} = 0.667 \operatorname{inch}^4$$

Displacement = $\delta = \frac{P \cdot L^3}{(3 \cdot E \cdot I)} = \frac{4000 \operatorname{1bs} \cdot 12^3 \operatorname{inch}}{(3 \cdot 29e^6 \operatorname{psi} \cdot 0.667 \operatorname{inch}^4)} = 0.119 \operatorname{inch}^4$

Bending Stress

Bending Moment = $M_y = P \cdot L = 4000 \text{ lbs} \cdot 12 \text{ inch} = 48000 \text{ in lbs}$ Maximum Bending Stress = $\sigma_b = \frac{M_y \cdot y}{I_y} = \frac{48000 \text{ in lbs} \cdot 1.0 \text{ inch}}{0.667 \text{ inch}^4} = 72000 \text{ psi}$

Horizontal shear stress

Maximum horizontal shear stress at the neutral axis = $\tau = \frac{V \cdot a \cdot y}{I_y \cdot t}$

$$\tau = \frac{4000 \, 1\text{bs} \cdot \, 1.0 \, \text{in}^2 \cdot 0.50 \, \text{in}}{0.667 \, \text{in}^4 \cdot 1 \, \text{in}} = 3000 \, \text{psi}$$



Suggested Exercise Steps

- 1. Create a new CATIA analysis document (.CATAnalysis).
- 2. Mesh globally with linear elements.
- 3. Apply a clamp restraint.
- 4. Apply a distributed force.
- 5. Compute the initial analysis.
- 6. Check global and local precision (animate deformation, adaptive boxes and extremas).
- 7. Change mesh to parabolic.
- 8. Compute the precise analysis.
- 9. Visualize final results.
- 10. Save the analysis document.



Step 1. Create a new CATIA analysis document





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Step 3. Apply a clamp restraint



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Step 3. Apply a clamp restraint





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Step 3. Apply a clamp restraint



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Step 5. Compute the initial analysis



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Step 5. Compute the initial analysis



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WS8-19

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Step 6. Check global and local precision



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WS8-20

MSC

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Step 6. Check global and local precision



MSC

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Step 6. Check global and local precision



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WS8-22

MSC

SOFTWARE

Step 7. Change mesh to parabolic







Step 8. Compute the precise analysis





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Step 8. Compute the precise analysis



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Step 8. Compute the precise analysis







Step 9. Visualize final results



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Step 9. Visualize final results



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Conclusions

 CATIA V5 GSA workbench is validated for a rectangular cantilever beam scenario. To be conservative, increase material strength to a minimum yield of 77000 psi for the described load case.

	Hand Calculations	.25" Parabolic Global Mesh, .025" sag
Global % Precision error	NA	1.25 %
Local % Precision error	NA	2.93 %
Error Estimate	NA	2.5e-7 Btu global
Translational Displacement	-0.119 inch	-0.121 inch (Z - direction)
Max Von Mises Stress	72000 psi	69400 - 76800 psi
Horizontal Shear Stress	3000 psi	3290 psi



Step 10. Save the analysis document





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List of Symbols and Definitions Greek letters.

- α = Angular acceleration (radians/sec/sec); included angle of beam curvature (degrees); form factor.
- δ = Perpendicular deflection (in.), bending (b) or shear (s).
- ε = Unit strain, elongation or contraction (in./in.)
- $\varepsilon_{s} =$ Unit shear strain (in./in.).
- ν = Poisson's ratio (aluminum = .346 usually, steel = .266 usually); unit shear force.
- ϕ = Unit angular twist (radians/linear inch); included angle; angle of rotation.
- σ = Normal stress, tensile or compressive (psi); strength (psi).
- $\sigma_b = Bending stress (psi).$
- $\sigma_{v} =$ Yield strength (psi).
 - τ = Shear stress (psi); shear strength (psi).
 - θ = Angle of twist (radians; 1 radian = 57.3 degrees); angle of rotation (radians); slope of tapered beam; any specified angle.



List of Symbols and Definitions

Letters.

- a = area of section where stress is desired or applied (in2)b = width of section (in)c = distance from neutral axis to extreme fiber (in) d = depth of section (in)e = eccentricity of applied load (in) f = force per linear inch (in)g = acceleration of gravity (386.4 inch/sec2)h = height (in)k = any specified constant or amplification factor m = massn = distance of section's neutral axis from ref axis (in)p = internal pressure (psi)r = radius (in); radius of gyration t = thickness of section (in)w = uniformly distributed load (lbs/linear inch)y = distance of area's center of gravity to neutral axis of entire section (in)
- A = area (in2); total area of cross-section E = modulus of elasticity, tension (psi) F = total force (lbs); radial force (lbs) I = moment of inertia (in4) J = polar moment of inertia (in4) L = length of member (in) M = bending moment (in-lbs) P = concentrated load (lbs) Q = shear center R = reaction (lbs) S = section modulus (in3) = I/c T = torque or twisting moment (in-lbs V = vertical shear load (lbs) W = total load (lbs); weight (lbs)
- C.G. = center of gravity D.O.F = degrees of freedom N.A. = neutral axis



WORKSHOP 8b

Z-SECTION CANTILEVER BEAM





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WORKSHOP 8b – Z-SECTION CANTILEVER BEAM





CAT509, Workshop 8b, March 2002

Problem Description

Bending and shear displacement

Moment of Inertia =
$$I_{y} = \frac{B \cdot D^{3} - ((D - (2 \cdot T))^{3} \cdot A)}{12} = \frac{0.5in \cdot 1.0in^{3} - ((1.0in - (2.0 \cdot 0.1in))^{3} \cdot 0.4in)}{12} = 0.0246 \text{ inch}^{4}$$

Bending Displacement = $\delta = \frac{P \cdot L^{3}}{(3 \cdot B \cdot I)} = \frac{1000 \text{ lbs} \cdot 6^{3} \text{ inch}}{(3 \cdot 10.15e^{6} \text{ psi} \cdot 0.0246 \text{ inch}^{4})} = 0.288 \text{ inch}$

Shear Displacement =
$$\partial = \frac{P \cdot L}{(B_s \cdot A)} = \frac{1000 \text{ lbs} \cdot 6 \text{ inch}}{(3.77e^6 \text{ psi} \cdot 0.1 \text{ inch}^2)} = 0.0159 \text{ inch}$$
 $\partial_{\text{Combined}} = 0.288in + 0.0159in = 0.304in$

Bending stress

Bending Moment =
$$M_y = P \cdot L = 1000 \text{ lbs} \cdot 6 \text{ inch} = 6000 \text{ in lbs}$$

Maximum Bending Stress = $\sigma_b = \frac{M_y \cdot y}{I_y} = \frac{6000 \text{ in lbs} \cdot 0.5 \text{ inch}}{0.0246 \text{ inch}^4} = 122000 \text{ psi}$



Suggested Exercise Steps

- 1. Create a new CATIA analysis document (.CATAnalysis).
- 2. Mesh globally with linear elements.
- 3. Apply a clamp restraint.
- 4. Apply a distributed force.
- 5. Compute the initial analysis.
- 6. Check global and local precision (animate deformation, adaptive boxes and extremas).
- 7. Change mesh to parabolic, possibly add local meshing.
- 8. Compute the precise analysis.
- 9. Visualize final results.
- 10. Save the analysis document.



Step 1. Create a new CATIA analysis document





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Step 2. Mesh globally with linear elements





WS8b-7

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Step 3. Apply a clamp restraint



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Step 4. Apply a distributed force



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Step 4. Apply a distributed force



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Step 5. Compute the initial analysis





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Step 7. Change mesh to parabolic





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Step 8. Compute the precise analysis





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Step 8. Compute the precise analysis





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Step 8. Compute the precise analysis





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WS8b-22



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CAT509, Workshop 8b, March 2002


Conclusions

 CATIA V5 GSA workbench is validated for a Z-section cantilever beam scenario. To be conservative, increase material strength to a minimum yield of 134000 psi for the described load case.

	Hand Calculations	.1 inch Parabolic Global Mesh, .01 inch sag
Global % Precision error	NA	2.38 %
Local % Precision error	NA	5.77 %
Error Estimate	NA	3.11e-7 Btu global
Translational Displacement	-0.304 inch	-0.308 inch (Z - direction)
Max Von Mises Stress	122000 psi	123000 - 134000 psi



Step 10. Save the analysis document





WORKSHOP 9

STRESS CONCENTRATION FOR A STEPPED FLAT TENSION BAR





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WORKSHOP 9 – STEPPED FLAT TENSION BAR







Problem Description

Approximate axial displacement

Axial Deformation =
$$\delta = \frac{P \cdot L}{E \cdot A} = \frac{10000 \text{ lbs} \cdot 3 \text{ inch}}{29 \text{ e}^6 \text{ psi} \cdot 0.125 \text{ inch}^2} = 0.0083 \text{ inch}$$

Stress configuration factor and axial stress

Stress Configuration Factor =
$$K_t = \frac{\sigma_{max}}{\sigma_{nom}}$$
 $\sigma_{nom} = \frac{P}{t \cdot d}$
 $\frac{D}{d} = \frac{1.5 \text{ inch}}{1.0 \text{ inch}} = 1.5$ $\frac{r}{d} = \frac{0.25 \text{ inch}}{1.0 \text{ inch}} = 0.25$ $K_t = 1.74 \text{ (R.E. Peterson1974 Figure 65)}$
Maximum normal tensile stress = $\sigma_{max} = \sigma_{nom} \cdot K_t = \frac{10000 \text{ lbs}}{0.125 \text{ inch} \cdot 1.0 \text{ inch}} \cdot 1.74$
 $\sigma_{max} = 80000 \text{ psi} \cdot 1.74 = 139200 \text{ psi}$



Suggested Exercise Steps

- 1. Create a new CATIA analysis document (.CATAnalysis).
- 2. Mesh globally with parabolic elements.
- 3. Apply a clamp restraint.
- 4. Apply a pressure force.
- 5. Compute the initial analysis.
- 6. Check global and local precision (animate deformation, adaptive boxes and extremas).
- 7. Change mesh size and add local meshing.
- 8. Compute the precise analysis.
- 9. Visualize final results.
- 10. Save the analysis document.



Step 1. Create a new CATIA analysis document



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WS9-6

MSC

SOFTWARE

Step 2. Mesh globally with parabolic elements





MSC

SOFTWARE

Step 3. Apply a clamp restraint



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Step 4. Apply a pressure force



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Step 5. Compute the initial analysis





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WS9-11

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MSC

SOFTWARE









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Step 7. Change mesh size and add local meshing



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Step 8. Compute the precise analysis





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Step 8. Compute the precise analysis







Step 8. Compute the precise analysis







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Conclusions

 CATIA V5 GSA workbench is validated for a stepped flat tension bar with shoulder fillets scenario.

	Hand Calculations	.1 inch Parabolic Global Mesh, .01 inch sag
Global % Precision error	NA	0.6 %
Local % Precision error	NA	0.47 %
Error Estimate	NA	7.04e-9 Btu global
Translational Displacement	0.0083 inch	0.00702 inch
Max Von Mises Stress	139200 psi	139407 psi



Step 10. Save the analysis document





WORKSHOP 9b

TORSION OF A SHAFT WITH A SHOULDER FILLET







Problem Description





<u>Material:</u> Steel Young Modulus = 29e6 psi Modulus of Rigidity = 12e6 psi Poisson Ratio = .266 Density = .284 lb_in3 Yield Strength = 36259 psi



Hand calculations

Maximum shear stress at the surface

Maximum Shear Stress =
$$\tau_{max} = \tau_{nom} \cdot K_{ts}$$
 $\tau_{nom} = \frac{16 \cdot T}{\pi \cdot d^3} = \frac{16 \cdot 1350 \text{ lb-inch}}{3.14 \cdot 0.63^3} = 27502 \text{ psi}$
 $K_{ts} = 1.42$ $\tau_{max} = 27502 \text{ psi} \cdot 1.42 = 39053 \text{ psi}$

Maximum angle of twist

Angle of twist (radians) =
$$\theta = \frac{T \cdot I}{J \cdot G}$$
 $J = 2 \cdot I = 2 \cdot \frac{\pi}{4} \cdot R^4 = 2 \cdot \frac{3.14}{4} \cdot 0.375^4$ inch = 0.031 inch⁴
 $\theta = \frac{1350 \text{ fb-inch} \cdot 5.01 \text{ inch}}{0.031 \text{ inch}^4 \cdot 12e^6} = 0.0182 \text{ radians} (1.04 \text{ degrees})$



Suggested Exercise Steps

- 1. Create a new CATIA analysis document (.CATAnalysis).
- 2. Mesh globally with linear elements.
- 3. Apply a clamp restraint.
- 4. Apply a moment force.
- 5. Compute the initial analysis.
- 6. Check global and local precision (animate deformation, adaptive boxes and extremas).
- 7. Change global and local mesh size.
- 8. Compute the precise analysis.
- 9. Visualize final results.
- 10. Save the analysis document.



Step 1. Create a new CATIA analysis document



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Step 2. Mesh globally with linear elements





WS9b-7

Step 3. Apply a clamp restraint





CAT509, Workshop 9b, March 2002

WS9b-8
Step 4. Apply a moment force



CAT509, Workshop 9b, March 2002



Step 5. Compute the initial analysis





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Step 7. Change global and local mesh size





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Step 8. Compute the precise analysis





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Step 8. Compute the precise analysis





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CATIA VS	- <mark>[ws9bShaft.CATAnalysis]</mark> eam <u>2</u> DM Eile Edit <u>Vi</u> ew Insert <u>I</u> ools <u>Wi</u> ndow <u>H</u> elp		
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	 Loads.1 Static Case Solution.1 Deform Generate Image Estimated local error Rotational displacement magnitude 	Strain full tensor component (nodal values) Strain principal tensor symbol Rotational displacement magnitude Rotational displacement vector Point force vector Point force text Moment vector Local strain energy Local strain energy density	8) (D' (C' (C' (C' (C' (C' (C' (C' (C' (C' (C
Add the Rotational displacement images. Steps: 1. Right click the Static Case Solution.1 in the features tree then select the Rotational displacement images	Rotational displacement vector Sensors.1 Adaptivity Process		



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WS9b-23



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Conclusions

 CATIA V5 GSA workbench is validated for a shaft with a shouldered fillet scenario.

	Hand Calculations	.06 inch Linear Global Mesh, .006 inch sag .03 inch Linear Local Mesh, .003 inch sag
Global % Precision error Local % Precision error	NA NA	19 % 24.1 %
Error Estimate	NA	4.93e7 Btu global
Translational Displacement	0.0182 radians	??
Stress Concentration Factor	1.42	1.45
Max Principal Shear Stress	39,053 psi (at shoulder radius)	34,800 – 35,600 psi at shoulder radius (design stress 88,500 psi)



Step 10. Save the analysis document





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WORKSHOP 10

ANNULAR PLATE





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CAT509, Workshop 10, March 2002



Problem Description

Shown below is a 2-D representation of the annular plate shown on the title page. The outer edge of the plate is simply supported and a uniform line load of 85 lb/in is applied a distance r_o from the center of the plate.

W W O simply supported simply supported а Ø 3.00 Ø.75

<u>Material:</u> Aluminum Young Modulus = 10e6 psi Poisson Ratio = .3 Density = .098 lb_in3 Yield Strength = 13778 psi

Design requirements:

 $\label{eq:constraint} \begin{array}{ll} Thickness, t = & 0.125 \text{ inch} \\ Annular Line Load Radius, r_0 = 0.75 \text{ inch} \\ Line Load, w = & 85 \text{ lb/inch} \end{array}$



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Hand calculations

• Displacement:

$$y = \frac{-wa^3}{D} \left(\frac{C_1 L_9}{C_7} - L_3 \right)$$

Plate constant:

$$D = \frac{Et^3}{12(1-v^2)}$$

Plate constants dependent on the ratio a/b:

$$C_{1} = \frac{1+v}{2}\frac{b}{a}\ln\frac{a}{b} + \frac{1-v}{4}\left(\frac{a}{b} - \frac{b}{a}\right)$$
$$C_{7} = \frac{1}{2}\left(1-v^{2}\right)\left(\frac{a}{b} - \frac{b}{a}\right)$$

Loading constants dependent upon the ratio a/r_o:

$$L_{3} = \frac{r_{0}}{a} \left\{ \left[\left(\frac{r_{0}}{a} \right)^{2} + 1 \right] \ln \frac{a}{r_{0}} + \left(\frac{r_{0}}{a} \right)^{2} - 1 \right\}$$
$$L_{9} = \frac{r_{0}}{a} \left\{ \frac{1+v}{2} \ln \frac{a}{r_{0}} + \frac{1-v}{4} \left[1 - \left(\frac{r_{0}}{a} \right)^{2} \right] \right\}$$



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- Hand calculations (cont.)
 - Plate constant:

D = 1788.576

- Plate constants dependent on the ratio a/b: $C_1 = 0.8815$ $C_7 = 1.7062$
- Loading constants dependent upon the ratio a/r_o : $L_3 = 0.0582$ $L_9 = 0.3346$
- Maximum vertical displacement:

Maximum bending stress:

Maximum banding stress = $\sigma = \frac{6 \cdot M}{t^2}$ $M = K_m \cdot w \cdot c = 0.5501 \cdot 85$ lbs/in $\cdot 1.5$ inch = 70.14 lbs $\sigma = \frac{6 \cdot 70.14 \text{ lbs}}{0.125^2 \text{ inch}} = 26934 \text{ psi}$



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Suggested Exercise Steps

- 1. Create a new CATIA analysis document (.CATAnalysis).
- 2. Mesh globally with parabolic elements.
- 3. Apply an advanced and isostatic restraint (simply supported).
- 4. Apply a line force density load.
- 5. Compute the initial analysis.
- 6. Check global and local precision (animate deformation, adaptive boxes and extremas).
- 7. Refine the mesh locally.
- 8. Compute the precise analysis.
- 9. Visualize final results.
- 10. Save the analysis document.



Step 1. Create a new CATIA analysis document



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WS10-7

MSC

SOFTWARE

Step 2. Mesh globally with parabolic elements





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Step 3. Apply an advanced restraint



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WS10-9

MSC

SOFTWARE

Step 3. Apply an isostatic restraint



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Step 4. Apply a line force density load





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Step 4. Apply a line force density load







Step 5. Compute the initial analysis





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MSC SOFTWARE

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CAT509, Workshop 10, March 2002

WS10-16

MSC

SOFTWARE
Step 6. Check global and local precision







Step 7. Refine the mesh locally





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Step 8. Compute the precise analysis



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WS10-20

SOFTWARE





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Conclusions

 CATIA V5 GSA workbench is validated for a annular flat circular plate scenario.

	Hand Calculations	.125 inch Parabolic Global Mesh, .013 inch sag .06 inch Local Mesh, .006 inch sag
Global % Precision error	NA	3.03 %
Local % Precision error	NA	3.76 %
Error Estimate	NA	3.02e-9 Btu global
Translational Displacement	-0.018 inch	-0.021 inch
Max Von Mises Stress	26934 psi	30736 psi



Step 10. Save the analysis document

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WORKSHOP 10...

OUTER EDGE SIMPLY SUPPORTED, INNER EDGE GUIDED OUTER EDGE SIMPLY SUPPORTED, INNER SIMPLE SUPPORTED OUTER EDGE SIMPLY SUPPORTED, INNER EDGE FIXED OUTER EDGE FIXED, INNER EDGE FREE





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WORKSHOP 10b

RECTANGULAR PLATE SMALL CONCENTRIC CIRCLE LOAD





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CAT509, Workshop 10b, March 2002



Problem Description

- All edges are simply supported.
- Uniform load over small concentric circle applied at the center.





Material: Aluminum Young Modulus = 29e6 psi Poisson Ratio = .3Density = .283 lb_in3 Yield Strength = 36000 psi

Design requirements:

Thickness, t =Radius of contact, $r_0 =$ Vertical Load, W =

0.1 inch 0.1 inch 500 lbs

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Hand calculations

Maximum Bending Stress:

Maximum Bending Stress (at center) =
$$\sigma_{max} = \frac{3 \cdot W}{2 \cdot \pi \cdot t^2} \cdot \left[(1 + \nu) \cdot \ln \frac{2 \cdot b}{\pi \cdot r_o^2} + \beta \right]$$

$$\sigma_{max} = \frac{3 \cdot 500 \text{ lbs}}{2 \cdot \pi \cdot 0.1^2 \text{ inch}} \cdot \left[(1 + 0.3) \cdot \ln \frac{2 \cdot 1.0 \text{ inch}}{\pi \cdot 0.1 \text{ inch}} + 0.958 \right] = 80317 \text{ psi}$$

Maximum Vertical Deflection:

Maximum Vertical Deflection =
$$y = \frac{\alpha \cdot W \cdot b^2}{E \cdot t^3} = \frac{-0.1805 \cdot 500 \text{ lbs} \cdot 1.0^2}{29e^6 \cdot 0.1^2} = 0.00311 \text{ inch}$$



Suggested Exercise Steps

- 1. Create a new CATIA analysis document (.CATAnalysis).
- 2. Mesh globally with parabolic elements.
- 3. Apply an advanced and isostatic restraint (simply supported).
- 4. Apply a force.
- 5. Compute the initial analysis.
- 6. Check global and local precision (animate deformation, adaptive boxes and extremas).
- 7. Refine the mesh locally with an adaptivity box.
- 8. Visualize final results.
- 9. Save the analysis document.



Step 1. Create a new CATIA analysis document



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Step 2. Mesh globally with parabolic elements





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Step 3. Apply an advanced and isostatic restraint



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Step 4. Apply a force



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plate.

Step 4. Apply a force



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Step 4. Apply a force



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Step 5. Compute the initial analysis





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Step 6. Check global and local precision



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WS10b-13

MSC

SOFTWARE

Step 6. Check global and local precision



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Step 7. Refine the mesh locally



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WS10b-15

MSC

SOFTWARE



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Conclusions

 CATIA V5 GSA workbench is validated for a rectangular flat plate with a uniform load over a small concentric circle scenario.

	Hand Calculations	.125 inch Parabolic Global Mesh, .013 inch sag .06 inch Local Mesh, .006 inch sag
Global % Precision error	NA	5.7 %
Local % Precision error	NA	3.8 %
Error Estimate	NA	4.93e-9 Btu global
Translational Displacement	-0.003 inch	-0.00328inch
Max Von Mises Stress	80317 psi	78900 psi



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Step 9. Save the analysis document

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WORKSHOP 10...

FOUR EDGES FIXED, TWO EDGES SIMPLY SUPPORTED - TWO EDGE FREE THREE EDGES FIXED TWO EDGES FIXED





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WORKSHOP 11

PRESS FIT









Problem Description

 Determine the contact pressure and the hoop stress for a class FN4 force fit (0.010 inch of interference on the diameter) of a steel plug into an aluminum cylinder.

0 Plug Material: Steel Young Modulus = 29e6 psiPoisson Ratio = .266Density = .284 lb_in3 х Yield Strength = 36259 psi 82.00f Outside Cylinder Material: Aluminum Young Modulus = 10.15e6 psi Poisson Ratio = .346Density = .098 lb_in3 Yield Strength = 13778 psi Note: parts are modeled net size



Hand calculations

Contact pressure due to 0.010 inch press fit on the diameter.

Assume the limit of interference due to a press fit = 0.010 inch on the diameter = δ

$$\partial = \left(\frac{r_{\text{inner optimizer 'P}}}{B_{\text{outer optimizer}}}\right) \cdot \left[\frac{(r_{\text{outer opt}}^2 + r_{\text{inner opt}}^2)}{(r_{\text{outer opt}}^2 - r_{\text{inner opt}}^2)} + v_{\text{outer}}\right] + \frac{r_{\text{inner opt}} \cdot p}{B_{\text{inner optimizer}}} \cdot (1 - v_{\text{inner}})$$

$$0.010in = \left(\frac{1.0_{\text{inner optimizer 'P}}}{10.15e^6_{\text{outer opt}} \cdot p}}\right) \cdot \left[\frac{(2.0_{\text{outer opt}}^2 + 1.0_{\text{inner opt}}^2)}{(2.0_{\text{outer opt}}^2 - 1.0_{\text{inner opt}}^2)} + 0.346_{\text{outer}}\right] + \frac{1.0_{\text{inner opt}} \cdot p}{29e^6_{\text{inner optimizer}}} \cdot (1 - 0.266_{\text{inner}})$$

$$0.010 = \frac{2.013 \cdot p}{10.15e^6} + \frac{30e^{-9} \cdot p}{29e^6}$$

$$p = \frac{0.010}{23e^{-8}} = 43478 \text{ psi}$$

Hoop stress at outside and inside diameters.

$$\sigma_{hoop} = p \cdot \frac{(r_{outer cylinder}^2 + r_{inner cylinder}^2)}{(r_{outer cylinder}^2 - r_{inner cylinder}^2)}$$

$$\sigma_{hoop} = 44782psi \cdot \frac{(2.0_{outer cyl}^2 + 1.0_{inner cyl}^2)}{(2.0_{outer cyl}^2 - 1.0_{inner cyl}^2)} = 43478 \cdot 1.667 = 72478 \text{ psi}$$



Suggested Exercise Steps

- 1. Open a ... CATProduct, and specify materials.
- 2. Create assembly constraints.
- 3. Create a new CATIA analysis document.
- 4. Apply analysis properties.
- 5. Mesh globally and locally.
- 6. Apply an isostatic restraint.
- 7. Compute the initial analysis.
- 8. Check global and local precision (animate deformation, adaptive boxes and extremas).
- 9. Visualize final results.
- 10. Save the analysis document.



Step 1. Open ... CATProduct and specify material



WS11-6

MSC

SOFTWARE



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Step 3. Create a new CATIA analysis document





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Step 4. Apply analysis properties





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Step 4. Apply analysis properties





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Step 6. Apply an isostatic restraint



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WS11-18

MSC X SOFTWARE

Step 7. Compute the initial analysis





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Step 8. Check global and local precision





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Step 8. Check global and local precision



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Step 8. Check global and local precision





WS11-22

MSC

SOFTWARE





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WS11-25



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WS11-26

MSC SOFTWARE



CAT509, Workshop 11, March 2002



Conclusions

CATIA V5 GSA workbench is validated for a press fit scenario.

		Hand Calculations	various Linear Global Mesh
Global % Precision error		NA	12.8 %
Local % Precision error		NA	12.7 %
Error Estimate		NA	1.03e-5 Btu global
Max Von Mises Stress		NA	104,765 psi
Hoop Stress		72,478 psi	74,900 – 76,300 psi
Pressure due to 0.010 interference		43,478 psi	46,000 – 47,300 psi



Step 10. Save the analysis document







WORKSHOP 12

FLAT PLATE COLUMN BUCKLING



CAT509, Workshop 12, March 2002

WS12-1





WORKSHOP 12 – FLAT PLATE COLUMN BUCKLING

Problem Description

- Rectangular plate under uniform edge compression
- Two short edges simply supported, two long edges free.
- Find the critical load when buckling begins.

<u>Material:</u> Aluminum Modulus of elasticity = 10.15e6 psi Poisson Ratio = .346 Density = .098 lb_in3 Yield Strength = 13778 psi

Design requirements: Thickness, t = Vertical Load, w =

0.1 inch 100 lbs/in





Hand calculations

Critical load of a long slender column:

Critical Load =
$$P_{cr} = \frac{\pi^2 \cdot E \cdot I_{min}}{L^2}$$
 $I_{min} = \frac{b \cdot t^3}{12} = \frac{1.0 \cdot 0.1^3}{12} = 0.00008333 \text{ inch}^4$
 $P_{cr} = \frac{\pi^2 \cdot 10.15e6 \text{ psi} \cdot 0.00008333 \text{ inch}^4}{4.0^2 \text{ inch}} = 522 \text{ lbs}$

 Verify model by checking deflection using the standard formula for a simply supported beam at both ends with uniform load over the entire span using a pressure of 100 psi (3D).





Suggested Exercise Steps

- 1. Create a new CATIA analysis document (.CATAnalysis).
- 2. Mesh globally with parabolic elements.
- 3. Create virtual parts and apply advanced restraints (simply supported).
- 4. Apply a force.
- 5. Insert a Buckling Case.
- 6. Setup static and buckling parameters.
- 7. Compute all (the static and buckling analysis).
- 8. Check global and local precision (animate deformation, adaptive boxes and extremas).
- 9. Visualize final results.
- 10. Save the analysis document.



Step 1. Create a new CATIA analysis document





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WS12-6
Step 2. Mesh globally with parabolic elements





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Step 3. Create virtual parts





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Step 3. Apply advanced restraints



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Step 3. Apply advanced restraints



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WS12-10

MSC SOFTWARE

Step 4. Apply a force





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Step 5. Insert a Buckling Case



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Step 6. Setup static and buckling parameters



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WS12-13

SOFTWARE

Step 7. Compute all



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Step 8. Check global and local precision





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Step 8. Check global and local precision



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WS12-16

MSC

SOFTWARE





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Conclusions

 CATIA V5 GSA workbench is validated for a flat plate column buckling scenario.

	Hand Calculations	.1 inch Parabolic Global Mesh, .01 inch sag
Global % Precision error	NA	1.58 %
Local % Precision error	NA	0 %
Error Estimate	NA	1.44e-9 Btu global
Critical Load	522 lbs	519 lbs
Model verification using simply supported beam displacement	0.394 inch	0.398 inch



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Step 10. Save the analysis document

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WORKSHOP 12...

FLAT PLATE BUCKLING, PINNED ALL FOUR EDGES FIXED ALL FOUR EDGES PINNED TWO EDGES, FIXED TWO EDGES

CANTILEVER PLATE LATERAL BUCKLING





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BICYCLE FENDER SURFACE MESHING



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WS13-1

m



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Problem Description

- Assume you are speeding down a steep hill at 30 mph. This causes a wind load of 5 psi on the fender.
- Determine the maximum stress and deflections.



<u>Material:</u> Bright Green Plastic Modulus of elasticity = 31.9e4 psi Poisson Ratio = .38 Density = .043 lb_in3

<u>Design requirements:</u> Thickness, t = 0.06 inch Wind Load, w = 5 psi



Suggested Exercise Steps

- 1. Start the Advanced Meshing Tools workbench (static analysis).
- 2. Specify global surface meshing parameters.
- 3. Add surface constraints.
- 4. Impose surface nodes.
- 5. Mesh the part.
- 6. Check mesh quality and repair.
- 7. Start the Generative Structural Analysis workbench.
- 8. Edit surface thickness.
- 9. Apply a clamp restraint.
- 10. Apply a pressure force.
- 11. Compute all.
- 12. Check global precision (animate deformation and find extremas).
- 13. Refine mesh and re-compute.
- 14. Visualize final results.
- 15. Save the analysis document.



Step 1. Start the Advanced Meshing Tools workbench



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Step 2. Specify global surface mesh parameters



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WS13-6

SOFTWARE

Step 3. Add surface constraints



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WS13-7

MSC

SOFTWARE

Step 4. Impose surface nodes







Step 5. Mesh the part



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WS13-9

MSC X SOFTWARE





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Step 7. Start the GSA workbench



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Step 8. Edit surface thickness







Step 9. Apply a clamp restraint





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Step 10. Apply a pressure force





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Step 11. Compute all



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WS13-19



Step 12. Check global precision



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WS13-20

MSC

SOFTWARE

Step 12. Check global precision



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WS13-21

Step 13. Refine mesh and re-compute



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WS13-22

SOFTWARE

Step 13. Refine mesh and re-compute



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WS13-23



Step 14. Visualize final results



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WS13-24

Step 14. Visualize final results



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WS13-25



Step 14. Visualize final results



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WS13-26



Conclusions

This fender requires stiffening in the mounting hole areas.

Global % Precision error	16.4%
Error Estimate	8.7e-6 Btu
Von Mises Stress	19,700 psi
Maximum Displacement	0.598 inch



Step 15. Save the analysis document

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WORKSHOP 14

KNOWLEDGEWARE





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Problem Description

- The preliminary design of the ATV Foot Peg must be completed as soon as possible and must meet the given structural requirements. The design must not exceed the material yield strength under loading and it must not deform in a manner causing interference with other parts of the vehicle.
- An initial static analysis of the Foot Peg has been completed (Workshop 2). To assist in our design iterations, we need to activate CATIA Knowledgeware capabilities to provide immediate feedback on the critical analysis parameters.





Suggested Exercise Steps

- 1. Open the existing document for the Foot Peg static analysis.
- 2. Create analysis sensors for maximum displacement and maximum stress.
- 3. Create a knowledge rule for maximum displacement.
- 4. Create a knowledge check for maximum stress.
- 5. Modify the Foot Peg design to meet requirements.
- 6. Compute the analysis for the modified design.
- 7. View results.



Step 1. Open the analysis document



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Step 2. Create analysis sensors



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Step 2. Create analysis sensors



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WS14-7



MSC

SOFTWARE



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Step 4. Create knowledge check



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Step 4. Create knowledge check



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Step 4. Create knowledge check



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Step 5. Modify Foot Peg design



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Step 5. Modify Foot Peg design



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Step 5. Modify Foot Peg design



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Step 6. Compute analysis



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Step 7. View results



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